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ABN 22 101 164 702 | ACN 101 164 702

December 15, 2014 Project No. 10530/2817 LWI/ms

# SITE INVESTIGATION REPORT

Client: NSW Land & Housing Corporation Address: 16-18 Stapleton Street, St. Marys

Proposed Development: Residential development

# **Site Description**

Approx. area (m2): 1910

Approx. fall: 2.5 to 3.0 metres to the west, good site drainage

Vegetation: Grass, shrubs and trees

Improvements: Vacant

# **Geology, Fieldwork Details and Subsurface Conditions**

The Penrith geological series sheet at a scale of 1:100,000 shows the site is underlain by Triassic Age Bringelly Shale of the Wianamatta Group. Rocks within this formation comprise shale, claystone and laminite.

Five boreholes were drilled and five Dynamic cone penetrometer (DCP) tests were carried out on November 29, 2014 at the locations shown on Drawing No. 14/2817. The subsurface conditions encountered are shown on the attached borehole logs. Explanation sheets and notes relating to geotechnical reports are also attached.

When making an assessment of the subsurface conditions across a site from a limited number of boreholes, there is the possibility that variations may occur between test locations. The data derived from the site investigation programme are extrapolated across the site to form a geological model and an engineering opinion is rendered about overall subsurface conditions and their likely behaviour with regard to the proposed development. The actual condition at the site may differ from those inferred, since no subsurface exploration programme, no matter how comprehensive, can reveal all subsurface details and anomalies.

The subsurface conditions consist of topsoil/fill overlying silty and gravelly clays and weathered shale. The topsoil/fill is present in all boreholes to depths of 0.3 to 0.5 metres. Silty and



gravelly clays are present to depths of 1.0 to 3.0 metres. The strength of these materials vary between firm to stiff and very stiff. In BH4, weathered shale underlies these soils and was observed to the depth of auger refusal, 1.2 metres.

No groundwater was observed in the boreholes during the fieldwork.

# **Laboratory Testing**

In order to assist with determining the site classification, two shrink/swell tests were carried out on representative samples retrieved from the site. The detailed test report is attached and summarised below:

Location	Depth	Material Description	Shrink/Swel
	(m)		l Index
			(% per ∆pF)
BH1	0.9-1.3	Light grey and orange brown silty clay	3.6
BH3	1.3-1.5	Brown and grey silty clay	1.0

# **Site Classification**

The classification has been prepared in accordance with the guidelines set out in the Residential Slabs and Footings" Code, AS2870 - 2011.

Because there are existing trees present, abnormal moisture conditions (AMC) prevail at the site. (Refer to Section 1.3.3 of AS2870).

Because of the AMC present, the site is classified a *problem site* (*P*). Provided the recommendations given below are adopted, the site may be reclassified *highly reactive* (*H2*).

Foundation design and construction consistent with this classification shall be adopted as specified in the above referenced standard and in accordance with the following design details.

### **Foundation Design and Construction**

Pad and/or strip footings founded in natural materials below the topsoil/fill, may be proportioned using an allowable bearing pressure of 100 kPa. The minimum depth of founding must comply with the requirements of AS2870. In order to overcome the presence of trees, the foundations are to be designed in accordance with Appendices H and CH of AS2870. The tree information is attached.

Piers founded in the very stiff materials may be proportioned using an allowable end bearing pressure of 450 kPa, provided their depth to diameter ratio exceeds a value of 4. An allowable



adhesion of 20 kPa may be adopted for the portion of the shaft in natural materials and below a depth of 0.5 metres. Piers that bear on the weathered shale may be proportioned using an allowable end bearing pressure of 700 kPa. When piers bear on weathered rock, adhesion in the overlying soils must be ignored.

In order to ensure the bearing values given can be achieved, care should be taken to ensure the base of the excavations are free of all loose material prior to concreting. To this end, it is recommended that all excavations be concreted as soon as possible, preferably immediately after excavating, cleaning, inspecting and approval. Pier excavations should not be left open overnight. The possibility of groundwater inflow needs to be considered when drilling the piers and pouring concrete.

The site is considered suitable for slab on ground construction provided due regard is given to the groundsurface slope.

During foundation construction, should the subsurface conditions vary to those inferred in this report, a suitably experienced geotechnical engineer should review the design and recommendations given above to determine if any alterations are required.

# **Soil Aggressiveness**

The exposure classification for the concrete has been determined for the onsite soils. The exposure classification is obtained from Tables 5.1 and 5.2 of AS2870-2011. In regards to the electrical conductivity, the laboratory test results have been multiplied by the appropriate factor to convert the results to EC<sub>e</sub>.

Detailed test reports are attached and summarised below, together with the exposure classification.

Sample	Electrical		рН	Sulfate	Exposure
No.	Conductivity (dS/m)			(ppm)	Classification
	EC <sub>1:5</sub>	EC <sub>e</sub>			
S1/2817	0.267	1.9	4.9	340	A2
S1/2817	0.276	1.9	4.6	720	A2
S1/2817	0.020	0.2	6.1	20	A1

The minimum concrete strength and reinforcement cover required for the various exposure classifications are given in Tables 5.3 and 5.4 of AS2870-2011.

Reference to DLWC (2002) "Site Investigations for Urban Salinity" indicates that  $EC_e$  values of 0.2 to 1.9 dS/m are consistent with the presence of non-saline soils.



### **Additional Comments**

Attention is drawn to Appendix B of AS2870 - 2011 regarding the need to properly maintain the foundations. Surface drainage should be provided to avoid the possibility of water ponding near the building and the finished ground surface should fall at least 50 mm over a distance of one metre away from the building.

The above classification has been made assuming that the maximum depth of filling placed in any building platform will be 400 mm and that all footings will bear in either natural ground or in controlled filling. Prior to the placement of any filling the existing surface should be stripped of all vegetation and topsoil.

The above classification is based on the soil profiles observed at the time of testing. If site works are undertaken, the classification of the actual building platform may vary across the site depending upon the extent of the cut and/or fill and the degree of compaction of any fill. The designer of the footing system must take the above factors into account.

If excavations for rainwater or detention tanks are to be made within 6 metres of the building foundations, advice should be sought regarding their effect on the foundations.

Placing absorption trenches on the high side of the property may create abnormal moisture conditions for the foundations (Refer to Section 1.3.3 of AS2870). This could have a negative effect on the foundation performance and more than likely alter the site classification provided above.

This report has been prepared assuming that no trees other than those noted will be present on the site. If future tree planting is planned, eg. there is a landscaping plan, their effect on the foundation performance must be considered.

This report has been prepared assuming the site development will be limited to one or two storey residential buildings. The information and interpretation may not be relevant if the design proposal changes (e.g. to a five-storey building involving major cuts during the site preparation). If changes occur, we would be pleased to review the report and advise on the adequacy of the investigation.

Yours faithfully,

Laurie Ihnativ, BE, MEngSc, MBA, FIE Aust.

Manager, SMEC Testing Services Pty Limited





**SMEC TESTING SERVICES Pty. Ltd.** 

Scale: Unknown

Date: December 2014

Client: NSW LAND & HOUSING CORPORATION

SITE INVESTIGATION

16-18 STAPLETON STREET, ST. MARYS

BOREHOLE AND PENETROMETER LOCATIONS

Project No. 10530/2817

Drawing No: 14/2817

### NOTES RELATING TO GEOTECHNICAL REPORTS

### Introduction

These notes have been provided to outline the methodology and limitations inherent in geotechnical reporting. The issues discussed are not relevant to all reports and further advice should be sought if there are any queries regarding any advice or report.

When copies of reports are made, they should be reproduced in full.

### **Geotechnical Reports**

Geotechnical reports are prepared by qualified personnel on the information supplied or obtained and are based on current engineering standards of interpretation and analysis.

Information may be gained from limited subsurface testing, surface observations, previous work and is supplemented by knowledge of the local geology and experience of the range of properties that may be exhibited by the materials present. For this reason, geotechnical reports should be regarded as interpretative rather than factual documents, limited to some extent by the scope of information on which they rely.

Where the report has been prepared for a specific purpose (eg. design of a three-storey building), the information and interpretation may not be appropriate if the design is changed (eg. a twenty storey building). In such cases, the report and the sufficiency of the existing work should be reviewed by SMEC Testing Services Pty Limited in the light of the new proposal.

Every care is taken with the report content, however, it is not always possible to anticipate or assume responsibility for the following conditions:

- Unexpected variations in ground conditions.
   The potential for this depends on the amount of investigative work undertaken.
- Changes in policy or interpretation by statutory authorities.
- The actions of contractors responding to commercial pressures.

If these occur, SMEC Testing Services Pty Limited would be pleased to resolve the matter through further investigation, analysis or advice.

### **Unforeseen Conditions**

Should conditions encountered on site differ markedly from those anticipated from the information contained in the report, SMEC Testing Services Pty Limited should be notified immediately. Early identification of site anomalies generally results in any problems being more readily resolved and allows reinterpretation and assessment of the implications for future work.

### **Subsurface Information**

Logs of a borehole, recovered core, test pit, excavated face or cone penetration test are an engineering and/or geological interpretation of the subsurface conditions. The reliability of the logged information depends on drilling/testing method, sampling and/or observation spacings and the ground conditions. It is not always possible or economic to obtain continuous high quality data. It should also be recognised that the volume or material observed or tested is only a fraction of the total subsurface profile.

Interpretation of subsurface information and application to design and construction must take into consideration the spacing of the test locations, the frequency of observations and testing, and the possibility that geological boundaries may vary between observation points.

Groundwater observations and measurements outside of specially designed and constructed piezometers should be treated with care for the following reasons:

- In low permeability soils groundwater may not seep into an excavation or bore in the short time it is left open.
- A localised perched water table may not represent the true water table.
- Groundwater levels vary according to rainfall events or season.
- Some drilling and testing procedures mask or prevent groundwater inflow.

The installation of piezometers and long term monitoring of groundwater levels may be required to adequately identify groundwater conditions.

# **Supply of Geotechnical Information or Tendering Purposes**

It is recommended tenderers are provided with as much geological and geotechnical information that is available and that where there are uncertainties regarding the ground conditions, prospective tenders should be provided with comments discussing the range of likely conditions in addition to the investigation data.

Client: Project:		nd Housing Cor		ВО	REHOLE NO.:	BH 1
Location:	Refer to Dra	wing No. 14/28	17 Logged: JK		Sheet 1 of 1	
W A T T A E B R L E	S A M P L E	<b>DEPTH</b> (m)	DESCRIPTION OF DRILLED PRODUCT  (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			SILTY CLAY: dark brown, medium plasticity, occasional gravel	CL	FIRM TO STIFF	D-M
	S1	0.5	TOPSOIL SILTY CLAY: red brown with light grey, medium to high plasticity	CL/CH	FIRM TO STIFF	М
	@ 0.6 m				STIFF TO	-
	U50	1.0	SILTY CLAY: light grey with orange brown, medium to high plasticity	CL/CH	VERY STIFF	M-D
		2.0	BOREHOLE DISCONTINUED AT 3.0 M			
NOTES:	D - disturbed WT - level o	d sample of water table or	free water N - Standard Penetration Test (SPT)	Contractor: Equipment Hole Diam		
				Angle fron	n Vertical (°) 0	

Client: Project:		nd Housing Cor		ВО	OREHOLE NO.:	BH 2
		wing No. 14/28			Sheet 1 of 1	
W A T T A E B R L E	S A M P L E	<b>DEPTH</b> (m)	DESCRIPTION OF DRILLED PRODUCT  (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R
			SILTY CLAY: dark brown, medium plasticity	CL	FIRM	D
			TOPSOIL  SILTY CLAY: red brown with light grey, medium to high plasticity	CL/CH	STIFF	D-M
		0.5				
		1.0				
		1.0				
		1.5	SILTY CLAY: light grey with orange brown, medium to high plasticity	CL/CH	VERY STIFF	M
		2.0				
		2.5				
		2.5				
NOTES	D 352 1		BOREHOLE DISCONTINUED AT 3.0 M	Contra	. CTC	
NOTES:	D - disturbed WT - level of	of water table or	U - undisturbed tube sample B - bulk sample free water N - Standard Penetration Test (SPT)  See explanation sheets for meaning of all descriptive terms and symbols	Contractor Equipment Hole Diam		
			· · · ·		n Vertical (°) 0	

Client: Project:		l and Housing Corporation Project No.: 10530/2817 apleton Street, St Marys Date: November 29, 2014			ВО	PREHOLE NO.:	ВН 3
		wing No. 14/28		Logged: JK		Sheet 1 of 1	
W A T T A E B R L E	S A M P L E	DEPTH (m)		DRILLED PRODUCT city, minor components, observations)	S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			SILTY CLAY: dark brown, low plasticity, trace of g	TOPSOIL/FILL	CL/CH	FIRM TO STIFF  FIRM TO STIFF	M-D
	U50	2.0	SILTY CLAY: light grey with orange brown, mediun	m to high plasticity	CL/CH	VERY STIFF	M-D
NOTES:	D - disturbed		BOREHOLE DISCONTINUED AT 3.0 M  U - undisturbed tube sample	B - bulk sample	Contractor	: STS	
		of water table or		N - Standard Penetration Test (SPT) ve terms and symbols	Equipment Hole Diam		

Client: Project:		nd Housing Cor		ВС	OREHOLE NO.:	BH 4
		wing No. 14/28			Sheet 1 of 1	
W A T T A E B R L E	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R
	S2 @ 0.4 m	(m)	TOPSOIL SILTY CLAY: orange brown/red brown with light grey, medium to high plasticity  WEATHERED SHALE/SANDSTONE: orange brown with light grey, fine grained  AUGER REFUSAL AT 1.2 M ON WEATHERED SHALE/SANDSTONE	CL/CH	FIRM TO STIFF	M-D D
NOTES:	D - disturbee	2.0	U - undisturbed tube sample B - bulk sample	Contracto	T. STS	
NOTES.		of water table or	ree water N - Standard Penetration Test (SPT)  See explanation sheets for meaning of all descriptive terms and symbols	Equipment Hole Dian	t: Christie neter (mm): 100 n Vertical (°) 0	

Client: Project:	NSW Land at				Project No.: 10530, Date: November		ВО	REHOLE NO.:	BH 5
	Refer to Dra				Logged: JK	29, 201 .		Sheet 1 of 1	
W A T T A E B R L E	S A M P L E S	DEPTH (m)	I.		DRILLED PRODUCT city, minor components, observations)		S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
	S3 @ 0.2 m	0.5		CLAY: dark brown, low plasticity, trace of g  CLAY: orange brown with red brown and lig  trace of ironstone gravel	TOPSOIL/FILL		CL/CH	VERY STIFF	D-M
		_ _ _	GRAVE	LLY CLAY: red brown, low plasticity, some	rironstone gravel		CL	VERY STIFF	D
		1.0							
		1.5							
		2.0							
		2.5							
			BOREH	OLE DISCONTINUED AT 3.0 M		ı			
NOTES:	D - disturbed WT - level o			U - undisturbed tube sample er	B - bulk sample N - Standard Penetration Test (SPT) re terms and symbols	Eq Ho	ole Diamo	STS Christie eter (mm): 100	

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# Dynamic Cone Penetrometer Test Report

Project: 16-18 STAPLETON STREET, ST. MARYS Project No.: 10530/2817

Client: NSW LAND & HOUSING CORPORATION

Report No.: 14/2788

Report Date: 15/12/2014

Address: Locked Bag 4009, Ashfield

......

Test Method: AS 1289.6.3.2

Page: 1 of 1

Site No.	P1	P2	P3	P4	P5	
Location	Refer to Drawing No. 14/2817	Refer to Drawing No. 14/2817	Refer to Drawing No. 14/2817	Refer to Drawing No. 14/2817	Refer to Drawing No. 14/2817	
Starting Level	Surface Level	Surface Level	Surface Level	Surface Level	Surface Level	
Depth (m)		Pen	etration Resistar	nce (blows / 150	mm)	
0.00 - 0.15	2	2	5	3	8	
0.15 - 0.30	4	2	2	5	12	
0.30 - 0.45	3	5	3	6	15	
0.45 - 0.60	3	8	3	10	22	
0.60 - 0.75	4	6	3	14	R	
0.75 - 0.90	4	6	5	22	*	
0.90 - 1.05	6	4	4	Refusal	*	
1.05 - 1.20	3	5	4		*	
1.20 - 1.35	7	5	6		*	
1.35 - 1.50	8	9	8		*	
1.50 - 1.65	10	10	9		*	
1.65 - 1.80	14	18	9		10	
1.80 - 1.95	9	22	10		17	
1.95 - 2.10	9	Refusal	12		22	
2.10 - 2.25	12		12		Refusal	
2.25 - 2.40	18		19			
2.40 - 2.55	22		22			
2.55 - 2.70	Refusal		Refusal			
2.70 - 2.85						
2.85 - 3.00						
3.00 - 3.15						
3.15 - 3.30						
3.30 - 3.45						
3.45 - 3.60						
3.60 - 3.75						

Remarks: \* Pre drilled prior to testing

Approved Signatory...

Technician: JK Laurie Ihnativ - Manager

Form: RPS26 Date of Issue: 07/07/11 Revision: 5

14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 Fax: (02)9756 1137 Email: smectesting@pacific.net.au

# Tree Heights and Type

Project: 16-18 Stapleton Street, St. Marys Project No. / STS No.: 10530/2817

Client: NSW Land & Housing Corporation Technician: JK

					1	
Tree No.	Canopy Radius	Distance from Tree Along Ground	Uphill / Level / Downhill	Height of Tree	Native	Growing / Mature
	(m)	(m)		(m)	(Y/N)	
T1	5		L	8	N	M
T2	3		L	6	Y	G
T3	2		L	15	N	M
T4	7		U	16	N	M
T5	10		U	30	Y	M

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# Shrink Swell Index Report

Project: 16 - 18 Stapleton Parade, St Marys

Client: NSW LAND & HOUSING CORPORATION

Address: Locked Bag 4009, Ashfield

Test Method: AS 1289.7.1.1

Project No.: 10530/5051C

Report No.: 14/2708 Report Date: 4/12/2014

Page: 1 of 1

Sampling Proceedure: AS 1289.1.3.1 Clause 3.1.3.2 - Thin Walled Sampler

STS / Sample No.		2817/1	2817/2		
San	nple Location	Borehole 1 Refer to Drawing	Borehole 3 Refer to Drawing		
Mate	rial Description	Silty Clay, red brown with light grey	Silty Clay, light grey with orange brown		
l	Depth (m)	0.9 - 1.3	1.3 - 1.5		
S	ample Date	29/11/2014	29/11/2014		
	Moisture Content (%)	25.7	15.7		
Shrink	Soil Crumbling	Nil	Nil		
Shr	Extent of Cracking	Fine Cracks	Fine Cracks		
	Strain (%)	5.8	0.6		
	Moisture Content Initial (%)	22.3	14.8		
Swell	Moisture Content Final (%)	21.3	18.6		
	Strain (%)	1.6	2.3		
Inert	Inclusions (%)	0.0	5.0		
Shrink	Swell Index (%)	3.6	1.0		

Remarks:

Approved Signatory......

Orlando Mendoza - Lab Manager

Technician: JH

Form: RPS41 Date of Issue: 08/07/11 Revision: 4



# **CERTIFICATE OF ANALYSIS**

Work Order : **ES1426666** Page : 1 of 4

Amendment : 1

Client : SMEC TESTING SERVICES PTY LTD Laboratory : Environmental Division Sydney

Contact : ALL REPORTS (ENQUIRIES) Contact : Client Services

Address : P O BOX 6989 Address : 277-289 Woodpark Road Smithfield NSW Australia 2164

WETHERILL PARK NSW, AUSTRALIA 2164

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 : --- Telephone
 : +61-2-8784 8555

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 : --- Facsimile
 : +61-2-8784 8500

Project : DOH : NEPM 2013 Schedule B(3) and ALS QCS3 requirement

Order number : 11627
C-O-C number : ----

 C-O-C number
 : --- Date Samples Received
 : 02-DEC-2014

 Sampler
 : JK
 Issue Date
 : 10-DEC-2014

Site : ----

Quote number : SY/593/14 No. of samples received : 7

Received : 7

No. of samples analysed : 7

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted. All pages of this report have been checked and approved for release.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results



NATA Accredited Laboratory 825

Accredited for compliance with ISO/IEC 17025.

### Signatories

This document has been electronically signed by the authorized signatories indicated below. Electronic signing has been carried out in compliance with procedures specified in 21 CFR Part 11.

Position	Accreditation Category
Inorganic Chemist	Sydney Inorganics
Inorganic Chemist	Sydney Inorganics
Inorganics Coordinator	Sydney Inorganics
	Inorganic Chemist

Address 277-289 Woodpark Road Smithfield NSW Australia 2164 PHONE +61-2-8784 8555 Facsimile +61-2-8784 8500 Environmental Division Sydney ABN 84 009 936 029 Part of the ALS Group An ALS Limited Company



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Work Order : ES1426666 Amendment 1

Client · SMEC TESTING SERVICES PTY LTD

Project : DOI

# ALS

### **General Comments**

The analytical procedures used by the Environmental Division have been developed from established internationally recognized procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are employed in the absence of documented standards or by client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contact for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.

LOR = Limit of reporting

^ = This result is computed from individual analyte detections at or above the level of reporting

This report has been amended and re-released to allow the reporting of additional analytical data.

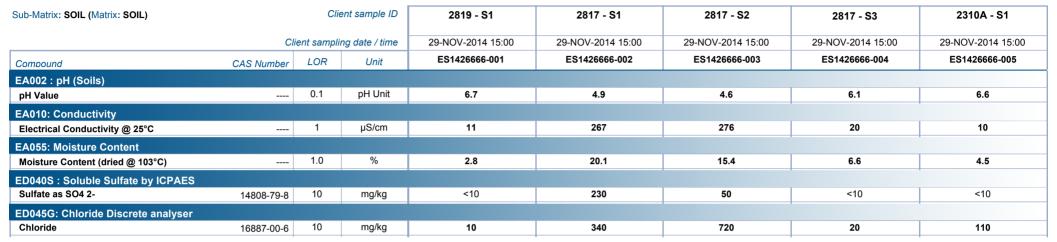
Page : 3 of 4

Work Order : ES1426666 Amendment 1

Client · SMEC TESTING SERVICES PTY LTD

Project : DOI

# Analytical Results





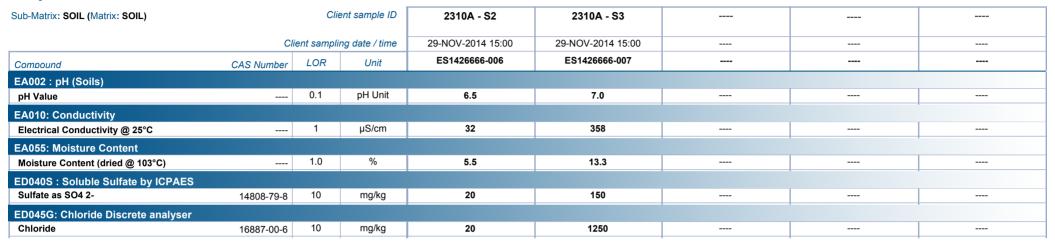
Page : 4 of 4

Work Order : ES1426666 Amendment 1

Client · SMEC TESTING SERVICES PTY LTD

Project : DOI

# Analytical Results





### E1. CLASSIFICATION OF SOILS

### E1.1 Soil Classification and the Unified System

An assessment of the site conditions usually includes an appraisal of the data available by combining values of engineering properties obtained by the site investigation with descriptions, from visual observation of the materials present on site.

The system used by SMEC in the identification of soil is the Unified Soil Classification system (USC) which was developed by the US Army Corps of Engineers during World War II and has since gained international acceptance and has been adopted in its metricated form by the Standards Association of Australia.

The Australian Site Investigation Code (AS1726-1981, Appendix D) recommends that the description of a soil includes the USC group symbols which are an integral component of the system.

The soil description should contain the following information in order:

### Soil composition

- SOIL NAME and USC classification symbol (IN BLOCK LETTERS)
- · plasticity or particle characteristics
- colour
- secondary and minor constituents (name estimated proportion, plasticity or particle characteristics, colour

### Soil condition

- moisture condition
- · consistency or density index

# Soil structure

• structure (zoning, defects, cementing)

### Soil origin

interpretation based on observation eg FILL, TOPSOIL, RESIDUAL, ALLUVIUM.

E1.2 Soil Composition

(a) Soil Name and Classification Symbol

The USC system is summarized in Figure E1.2.1. The primary division separates soil types on the basis of particle size into:

- Coarse grained soils more than 50% of the material less than 60 mm is larger than 0.06 mm (60 μm).
- Fine grained soils more than 50% of the material less than 60 mm is smaller than 0.06 mm (60  $\mu$ m).

Initial classification is by particle size as shown in Table E1.2.1. Further classification of fine grained soils is based on plasticity.

TABLE E1.2.1 - CLASSIFICATION BY PARTICLE SIZE

NAME	SUB-DIVISION	SIZE
Clay (1)		< 2 μm
Silt (2)		2 μm to 60 μm
Sand	Fine Medium Coarse	60 μm to 200 μm 200 μm to 600 μm 600 μm to 2 mm
Gravel (3)	Fine Medium Coarse	2 mm to 6 mm 6 mm to 20 mm 20 mm to 60 mm
Cobbles (3)		60 mm to 200 mm
Boulders (3)		> 200 mm

Where a soil contains an appropriate amount of secondary material, the name includes each of the secondary components (greater than 12%) in increasing order of significance, eg sandy silty clay.

Minor components of a soil are included in the description by means of the terms "some" and "trace" as defined in Table E1.2.2.

TABLE E1.2.2 - MINOR SOIL COMPONENTS

TERM	DESCRIPTION	APPROXIMATE PROPORTION (%)
Trace	presence just detectable, little or no influence on soil properties	0-5
Some	presence easily detectable, little influence on soil properties	5-12

The USC group symbols should be included with each soil description as shown in Table E1.2.3

TABLE E1.2.3 - SOIL GROUP SYMBOLS

SOIL TYPE	PREFIX	
Gravel	G	
Sand	S	
Silt	M	
Clay	С	
Organic	О	
Peat	Pt	

The group symbols are combined with qualifiers which indicate grading, plasticity or secondary components as shown on Table E1.2.4

TABLE E1.2.4 - SOIL GROUP QUALIFIERS

	_
SUBGROUP	SUFFIX
Well graded	W
Poorly Graded	P
Silty	M
Clayey	C
Liquid Limit <50% - low to medium plasticity	L
Liquid Limit >50% - low to medium plasticity	Н

### (b) Grading

"Well graded" Good representation of all

particle sizes from the largest

to the smallest.

"Poorly graded" One or more intermediate

sizes poorly represented

"Gap graded" One or more intermediate

sizes absent

"Uniformly graded" Essentially single size

material.

### (c) Particle shape and texture

The shape and surface texture of the coarse grained particles should be described.

**Angularity** may be expressed as "rounded", "sub-rounded", "sub-angular" or "angular".

Particle **form** can be "equidimensional", "flat" or elongate".

**Surface texture** can be "glassy", "smooth", "rough", pitted" or striated".

### (d) Colour

The colour of the soil should be described in the moist condition using simple terms such as:

> Black White Grey Red Brown Orange Yellow Green Blue

These may be modified as necessary by "light" or "dark". Borderline colours may be described as a combination of two colours, eg. red-brown.

For soils that contain more than one colour terms such as:

Speckled Very small (<10 mm dia) patches</li>

Mottled Irregular

• Blotched Large irregular (>75 mm dia)

Streaked Randomly oriented streaks

### (e) Minor Components

Secondary and minor components should be individually described in a similar manner to the dominant component.

### E1.3 Soil Condition

### (a) Moisture

Soil moisture condition is described as "dry", "moist" or "wet".

The moisture categories are defined as:

Dry (D) - Little or no moisture evident. Soils are running. Moist (M) - Darkened in colour with cool feel. Granular soil particles tend to adhere. No free water evident upon remoulding of cohesive soils.

In addition the moisture content of cohesive soils can be estimated in relation to their liquid or plastic limit.

(b) Consistency

Estimates of the consistency of a clay or silt soil may be made from manual examination, hand penetrometer test, SPT results or from laboratory tests to determine undrained shear or unconfined compressive strengths. The classification of consistency is defined in Table E1.3.1.

TABLE E1.3.1 - CONSISTENCY OF FINE-GRAINED SOILS

TERM	UNCONFINED	FIELD	
	STRENGTH	IDENTIFICATION	
	(kPa)		
Very Soft	<25	Easily penetrated by fist. Sample exudes between fingers when squeezed in the fist.	
Soft	25 – 50	Easily moulded in fingers. Easily penetrated 50 mm by thumb.	
Firm	50 – 100	Can be moulded by strong pressure in the fingers. Penetrated only with great effort.	
Stiff	100 – 200	Cannot be moulded in fingers. Indented by thumb but penetrated only with great effort.	
Very Stiff	200 – 400	Very tough. Difficult to cut with knife. Readily indented with thumb nail.	
Hard	>400	Brittle, can just be scratched with thumb nail. Tends to break into fragments.	

Unconfined compressive strength as derived by a hand penetrometer can be taken as approximately double the undrained shear strength  $(q_u=2\ c_u)$ .

### (c) Density Index

The insitu density index of granular soils can be assessed from the results of SPT or cone penetrometer tests. Density index should not be estimated visually.

TABLE E1.3.2 - DENSITY OF GRANULAR SOILS

TERM	SPT N	STATIC	DENSITY
	VALUE	CONE	INDEX
		VALUE	(%)
		q <sub>c</sub> (MPa)	
Very Loose	0 – 3	0 - 2	0 - 15
Loose	3 – 8	2 - 5	15 - 35
Medium Dense	8 - 25	5 - 15	35 - 65
Dense	25 - 42	15 - 20	65 - 85
Very Dense	>42	>20	>85

### E1.4 Soil Structure

### (a) Zoning

A sample may consist of several zones differing in colour, grain size or other properties. Terms to classify these zones are:

Layer - continuous across exposure or sample

Lens - discontinuous with lenticular shape

Pocket - irregular inclusion

Each zone should be described, their distinguishing features, and the nature of the interzone boundaries.

### (b) Defects

Defects which are present in the sample can include:

- fissures
- roots (containing organic matter)
- tubes (hollow)
- casts (infilled)

Defects should be described giving details of dimensions and frequency. Fissure orientation, planarity, surface condition and infilling should be noted. If there is a tendency to break into blocks, block dimensions should be recorded

# E1.5 Soil Origin

Information which may be interpretative but which may contribute to the usefulness of the material description should be included. The most common interpreted feature is the origin of the soil. The assessment of the probable origin is based on the soil material description, soil structure and its relationship to other soil and rock materials.

### Common terms used are:

"Residual Soil" - Material which appears to have been derived by weathering from the underlying rock. There is no evidence of transport.

"Colluvium" - Material which appears to have been transported from its original location. The method of movement is usually the combination of gravity and erosion.

"Landslide Debris" - An extreme form of colluvium where the soil has been transported by mass movement. The material is obviously distributed and contains distinct defects related to the slope failure. "Alluvium" - Material which has been transported essentially by water. Usually associated with former stream activity.

"Fill" - Material which has been transported and placed by man. This can range from natural soils which have been placed in a controlled manner in engineering construction to dumped waste material. A description of the constituents should include an assessment of the method of placement.

### E1.6 Fine Grained Soils

The physical properties of fine grained soils are dominated by silts and clays.

The definition of clay and silt soils is governed by their Atterberg Limits. Clay soils are characterised by the properties of cohesion and plasticity with cohesion defines as the ability to deform without rupture. Silts exhibit cohesion but have low plasticity or are non-plastic.

The field characteristics of clay soils include:

- dry lumps have appreciable dry strength and cannot be powdered
- volume changes occur with moisture content variation
- feels smooth when moist with a greasy appearance when cut.

The field characteristics of silt soils include:

- dry lumps have negligible dry strength and can be powdered easily
- dilatancy an increase in volume due to shearing is indicted by the presence of a shiny film of water after a hand sample is shaken. The water disappears upon remoulding. Very fine grained sands may also exhibit dilatancy.
- low plasticity index
- · feels gritty to the teeth

### E1.7 Organic Soils

Organic soils are distinguished from other soils by their appreciable content of vegetable matter, usually derived from plant remains.

The soil usually has a distinctive smell and low bulk density.

The USC system uses the symbol Pt for partly decomposed organic material. The O symbol is combined with suffixes "O" or "H" depending on plasticity.

Where roots or root fibres are present their frequency and the depth to which they are encountered should be recorded. The presence of roots or root fibres does not necessarily mean the material is an "organic material" by classification.

Coal and lignite should be described as such and not simply as organic matter.